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Intensification of the Bitumen Production Process

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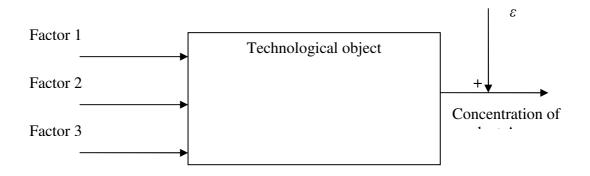
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The intensification and automation of deasphalting units with propane is considered from the point of view of the possibility of obtaining deasphalting asphalt, which is stable in physical and chemical properties, in particular, in terms of softening and flash points. The use of deasphalting asphalt as a component of compounded bitumen or as a raw material for the production of oxidized bitumen imposes certain requirements on the stability of its (asphalt) properties. On the basis of the research carried out by the authors and the analysis of the operation of existing installations, the following schemes of automatic control and regulation of the main units of the process of deasphalting with propane have been proposed [1,2: 45-46, 61].

The purpose of the experiment is to determine a new direction of the gradient for the steep ascent procedure. This constitutes the content of the second cycle of the procedure. By analogy with the above, we select the intervals of variation for each of the factors and fill in the table of the values of the factors during the experiment. Next, we draw up an experiment plan, implement it and place the results in the experiment implementation table.

Table 1

Factor name Units		Minimum allowed value	Maximum allowable value	Process implementation mode
1) Temperature	Hail	30	120	50
Pressure	kgf / cm2	1,5	3,5	2
Stirrer rotation speed	rpm	40	70	45



The value of the variation interval for each of the factors is limited from below, first of all, by the errors of instruments and devices with which the values of the factors are measured and set during experimentation. No specific statements can be made regarding the upper bound [3,4: 65, 32].

However, you can accept: $0.05 \cdot x_{0j} \le \Delta_j \le 0.07 \cdot x_{0j}$,

where Δ_j - factor variation interval x_j ; x_{jB} - maximum allowable value x_j ; x_{jH} - minimum allowable value x_j ;

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Thus, we have

$$\Delta_1 = 0.05 \cdot (120 - 30) = 4.5$$
, that more $0.05 \cdot 50 = 2.5$

$$\Delta_2 = 0.05 \cdot (3.5 - 1.5) = 0.1$$
 , what is equal $0.05 \cdot 2 = 0.1$

$$\Delta_3 = 0.05 \cdot (70 - 40) = 1.5$$
, which is less $0.05 \cdot 45 = 2.25$

Table 2 Table of factor values for experimentation

№	Factor name	One. Rev.	Lower level	Top level	
1	2) Temperature	Град	47,5	52,5	
2	3) Pressure	Кгс/см	1,9	2,1	
3	Stirrer rotation speed	Об./мин.	43,5	46,5	

After constructing a plan for a full factorial experiment 23, conducting randomization and implementing experiments, we have:

Table 3

4) Experiment Implementation Table

		Experiment plan						Result			
No	5) Temperature		P	ressure	Rotational speed мешалки		Concentration				
110	code	significant	code	significant	code	significant	Por. №	meaning	Por №	meaning	
1	-1 —	47,5	-1	1,9	-1	43,5	7	41,53	1	37,61	
2	+1	52,5	-1	1,9	-1	43,5	5	42,43	3	42,14	
3	-1	47,5	+1	2,1	- 1	43,5	9	45,00	13	42,40	
4	+1	52,5	+1	2,1	-1	43,5	6	46,81	16	46,41	
5	-1	47,5	-1	1,9	+1	46,5	4	45,27	11	43,50	
6	+1	52,5	-1	1,9	+1	46,5	2	46,00	12	45,30	
7	-1	47,5	+1	2,1	+1	46,5	14	48,41	15	48,02	
8	+1	52,5	+1	2,1	+1	46,5	8	49,10	10	50,03	

The result of calculating the estimates of the regression coefficients and checking their significance are summarized in the table:

Table 4 Model Coefficient Estimation Table

Estimation of coefficients.	Score value	The value of T statistics	$t_{\kappa p}$	Hypothesis test result
\overline{b}_0	45,0013	138,65	2.31	1
$ar{b}_{ m l}$	1,0263	3,16	2.31	1
\bar{b}_2	2,0288	6,25	2.31	1
\overline{b}_3	1,9600	6,03	2.31	1
\overline{b}_{12}	0,0313	0,096	2.31	0
\bar{b}_{13}	-0,3800	1,17	2.31	0
\bar{b}_{23}	-0,0850	0,26	2.31	0

Thus, the model in normalized variables is:

$$y = 45 + 1.02 \cdot x_1 + 2.03 \cdot x_2 + 1.96 \cdot x_3$$

Fisher's criterion $F = S_{a\partial}^2 / S_e^2$

$$F=2,76$$
, $v_1=4$, $v_2=8$,

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According to the Fisher distribution table, we determine $S_{\kappa\rho} = 3,84$

Thus, the resulting model is adequate. In natural variables, the model is:

$$y = 45 + 1.02 \cdot (x_1 - 50) / 4.5 + 2.03 \cdot (x_2 - 2) / 0.1 + 1.96 \cdot (x_3 - 45) / 1.5$$

After reducing similar terms, we have:

$$y = -65,73 + 0,23 \cdot x_1 + 20,3 \cdot x_2 + 1,3 \cdot x_3$$

where x_1 – temperature in ${}^{0}C$; concentration of product A in%.

 x_2 – pressure, кгс/см²; x_3 – stirrer rotation speed in rpm;

Table 5

Model: $y = 213,16 + 0,22 \cdot x_1 - 84,8 \cdot x_2 + 0,3 \cdot x_3$									
Option	Option number 1		Factors			results			
Название		Temperature	Pressure	Speed time. agitators	Concentration of product A		oduct A		
start	starting point		3,3	62,28					
Wo	ork step	2,25	-0,42	0,34					
Step	Experiment				By model	Experiments		Wednesday	
Number	type.				\overline{y}	<i>y</i> ₂	y_I	Y	
15	M	79,25	2,88	62,62	5,15				
16	M	81,5	2,46	62,96	41,37				
17	P	83,75	2,04	63,30	77,58	69.58	69.03		
18	M	86	1,62	63,64					
19	P	88,25	1,2	63,98		47.98	46.81		
20	M	90,5	0,78	64,32					
21	P	92,75	0,36	64,66		15.97	14.74		

At the 17th step, we find a new extremum. This marks the completion of the second cycle of the steep ascent procedure. Now it is necessary to re-plan and implement a complete factorial experiment in the area, the center of which has the coordinates:

Temperature = 83.75 $^{\circ}C$:

 $Pressure = 2.04 \ \kappa cc/cm^2$;

Stirrer rotation speed = 63,30 rpm.

By analogy with the above, we select the intervals of variation for each of the factors and fill in the table of the values of the factors during the experiment.

Next, we draw up an experiment plan, implement it and place the results in the experiment implementation table.

We choose the interval of variation:

$$\Delta_1 = 0.05 \cdot (120 - 30) = 4.5$$
, that more $0.05 \cdot 83.75 = 4.19$

$$\Delta_2 = 0.05 \cdot (3.5 - 1.5) = 0.1$$
, which is less $0.05 \cdot 2.04 = 0.1$

$$\Delta_3 = 0.05 \cdot (70 - 40) = 1.5$$
, which is less $0.05 \cdot 63.3 = 3.16$

Table of factor values for experimentation



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Table 6

No	Factor name	Unified measurement.	Lower level	Top level	
1	6) Temperature	Hail	79,25	88,25	
2	Pressure	кгс/см ²	1,94	2,14	
3	Stirrer rotation speed	Rpm	61,8	64,8	

After constructing a plan for a full factorial experiment 23, conducting randomization and implementing experiments, we have:

Thus, the resulting model contains a linear component, therefore, the maximum concentration value should be at the boundary of the experimental area. The average value of the output controlled parameter is maximum at the maximum values of the input factors (Y=45,00%). Therefore, it is possible to increase the concentration of product A by changing the process conditions. In this regard, it is advisable to use a steep ascent procedure to optimize the process.

References

1.	Гунн,	Р.Б.	Нефтяные	битумы.	M.:	Химия,
	1973. – 432 c.					

- 2. Юсупова Н.К. Технология получения строительного битума из нефтяных шламов. Дисс. докт.фил. (PhD) технических наук, Ташкент-2021. - 101 с.
- 3. Кемалов А.Ф. Использование отходов нефтехимических производств для интенсификации процесса получения нефтяных битумов; автореф. дис. канд. хим. наук / А.Ф. Кемалов. - Казань, 1995. - С.15.
- 4. Ахметова Р.С. Структурообразование и улучшение технологии получения битумов, применяемых в дорожном строительстве: Дис.канд. техн. наук. М. 1967. - 180 с.